

# MODELING A BIORETENTION BASIN AND VEGETATED SWALE WITH TRAPEZOIDAL CROSS-SECTIONAL AREAS USING SWMM'S LID CONTROL MODULE

Presented at the ICSWMM 2020 for  
**Polytechnique Montreal University, QC, CAN**

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**Introduction**

**Design of LID in  
PCSWMM**

**Input Field  
Data**

**Parameter  
Selection**

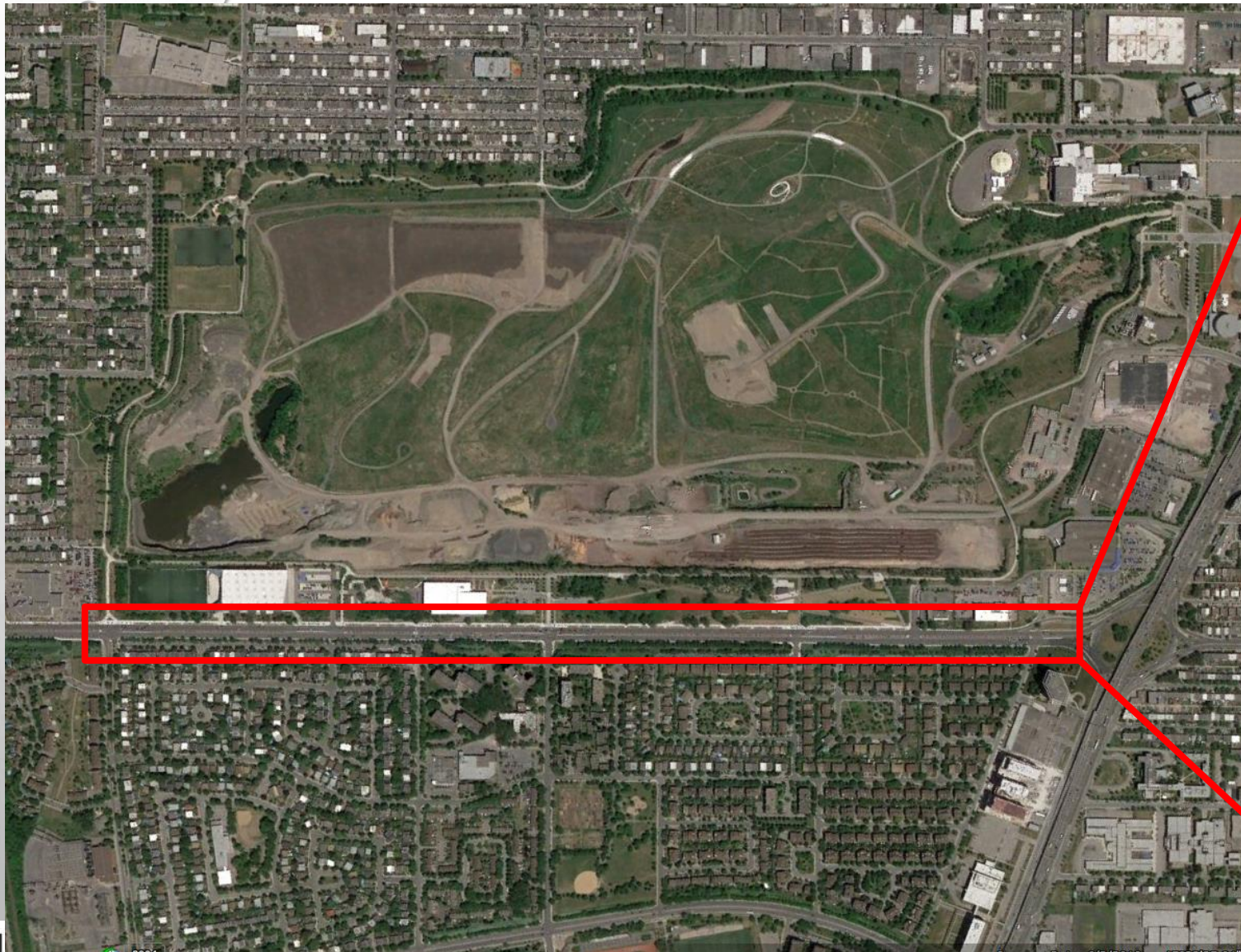
**Sensitivity  
Analysis**

**Calibration  
Results**

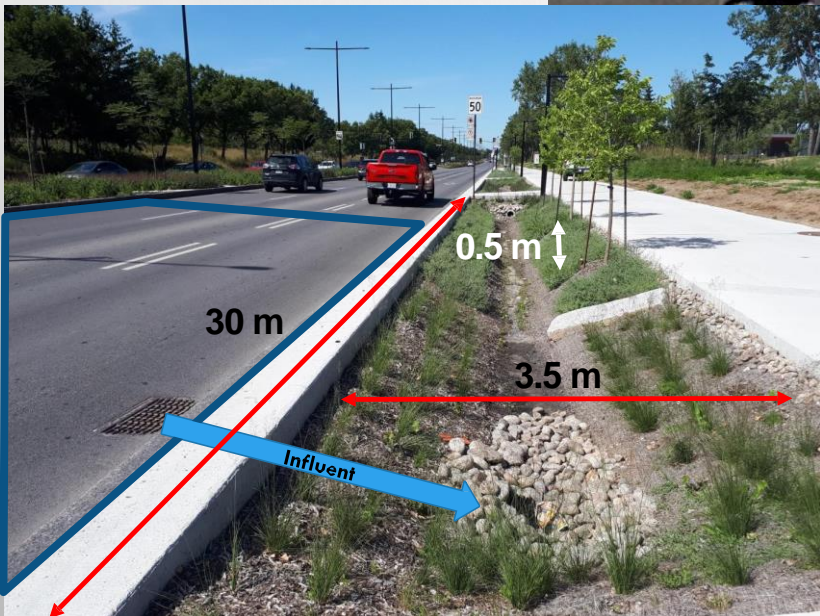
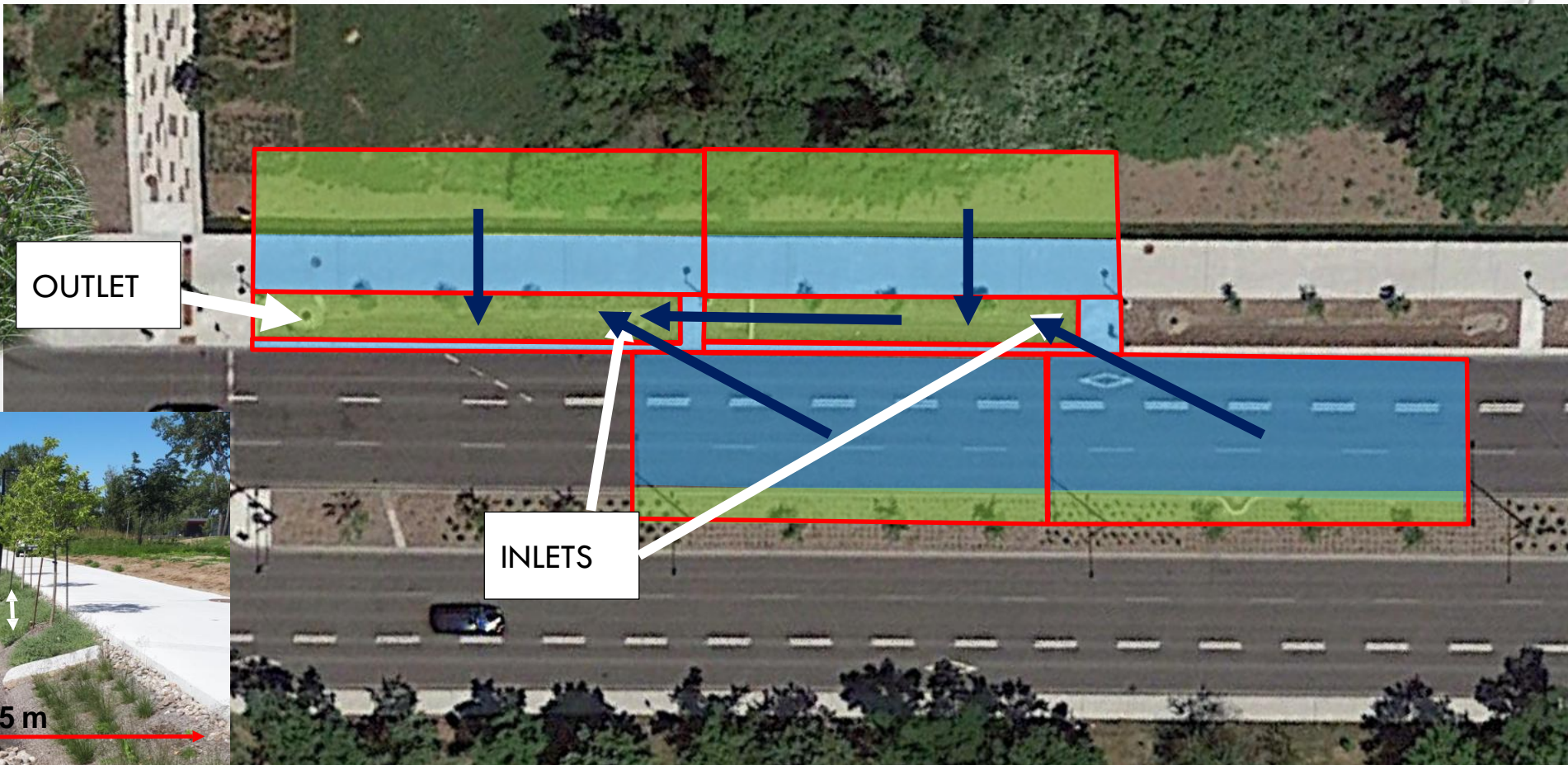
**Calibration**

**What is next?  
Continued  
troubleshooting?**



# PAPINEAU PROJECT— PLAN VIEW



# PAPINEAU PROJECT- PLAN VIEW



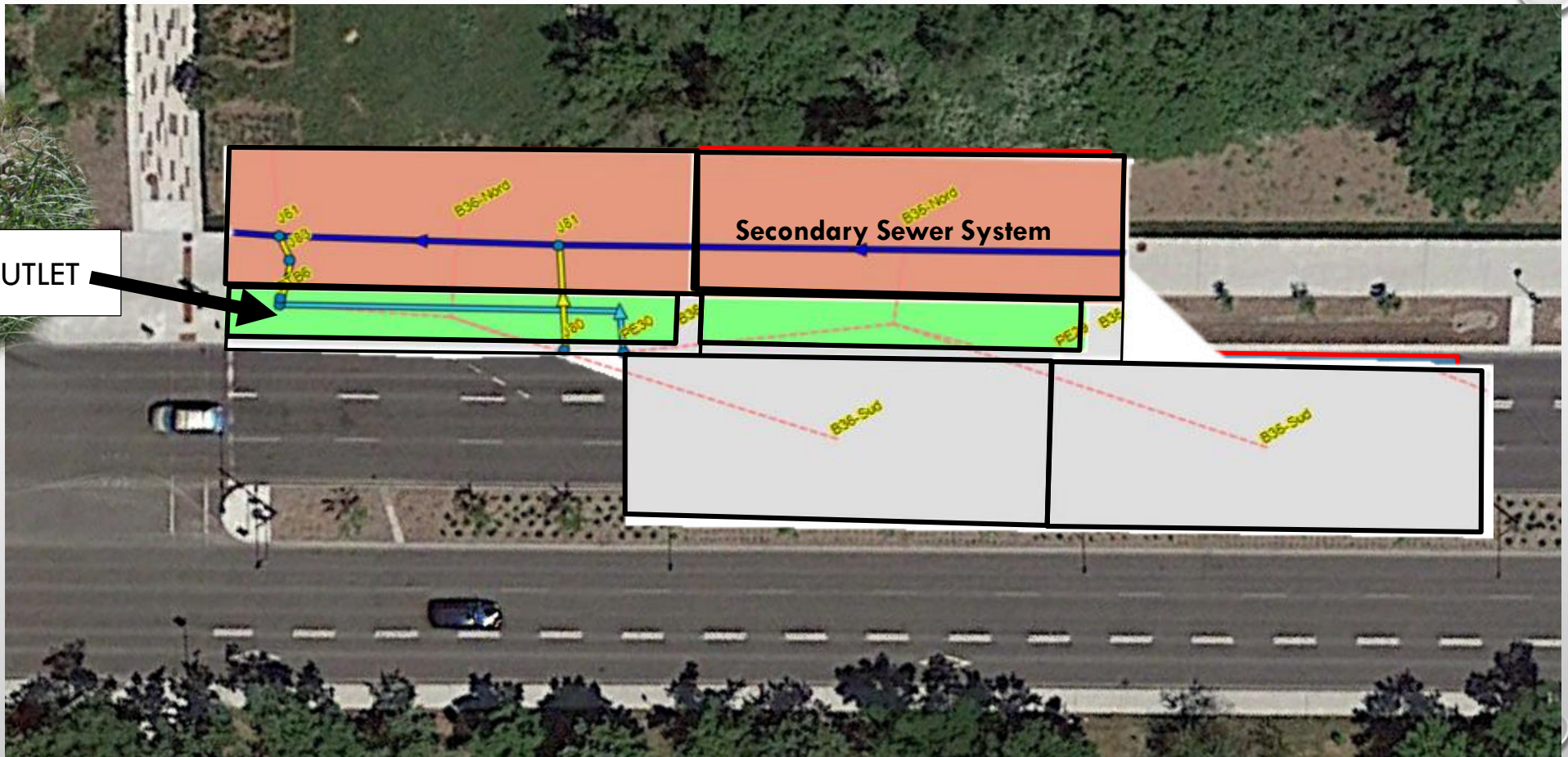
## LEGEND

	= IMPERVIOUS
	= PERVIOUS

# DESIGN OF LIDS IN PCSWMM – PLAN VIEW



OUTLET






- The drainage area to LID surface is approximately 4.5:1

## Assumptions

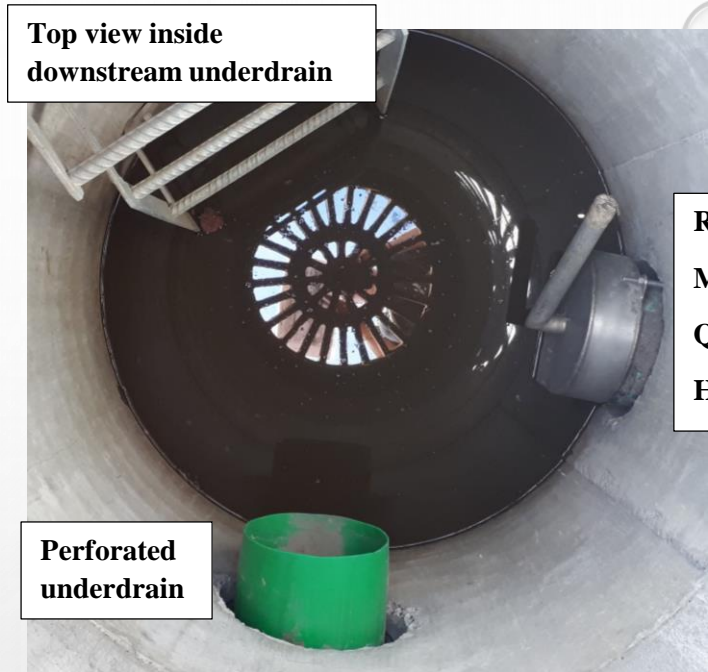
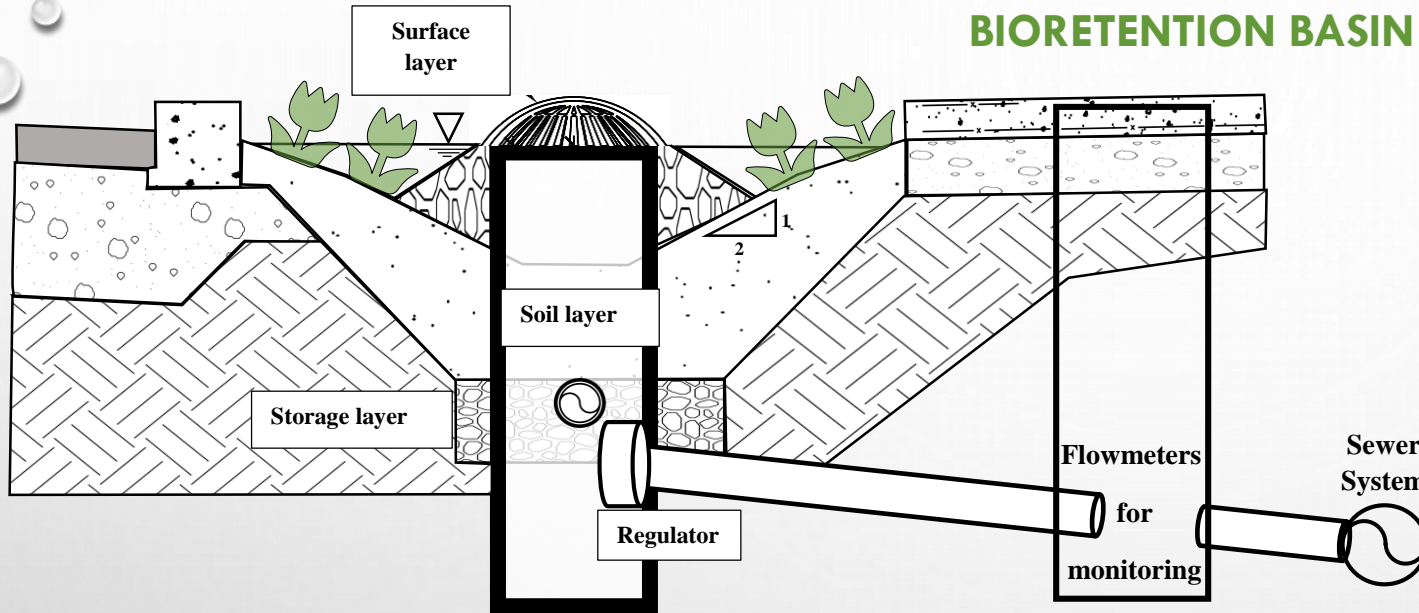
- No catch basin capacity limitations were considered

## LEGEND

	= SIDEWALK + GRASS
	= LID UNITS
	= STREET + MEDIAN

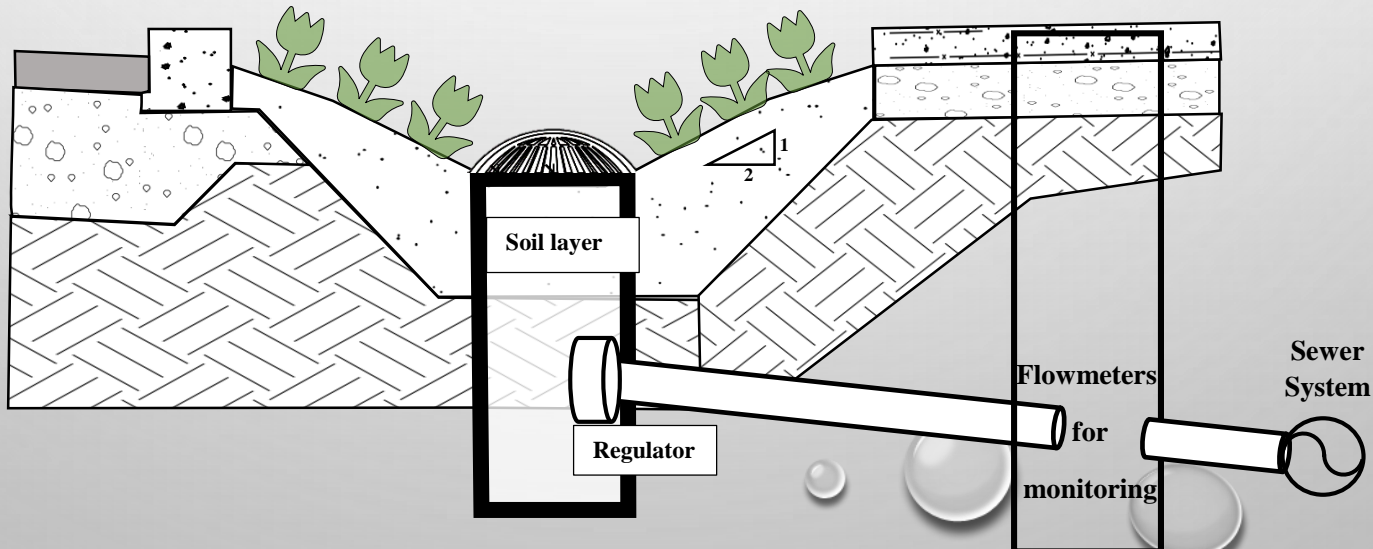
# CROSS-SECTIONAL VIEW OF LID STRUCTURES

## BIORETENTION BASIN

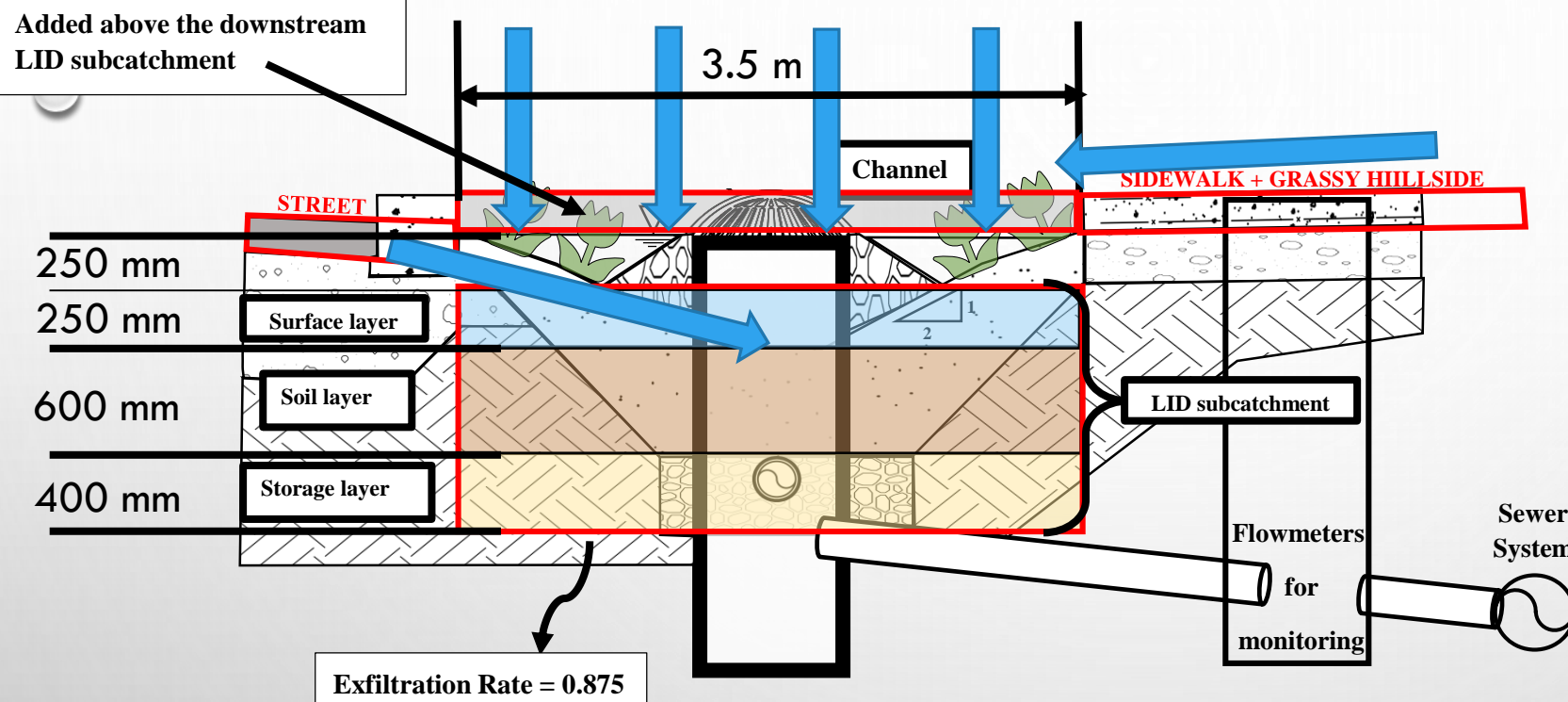


**Regulator**  
 Max  
 $Q = 4.5 \text{ L/s}$   
 $H = 1.8 \text{ m}$

## VEGETATED SWALE



## BIORETENTION BASIN AS MODELLED BY SWMM



### ERRORS WHEN USING THE REAL AREA:

- Potential storage volume of **SURFACE LAYER**
  - Real =  $50.26 \text{ m}^3$
  - SWMM =  $101.84 \text{ m}^3$
- Volume of **STORAGE LAYER**
  - Real =  $32.80 \text{ m}^3$
  - SWMM =  $81.47 \text{ m}^3$

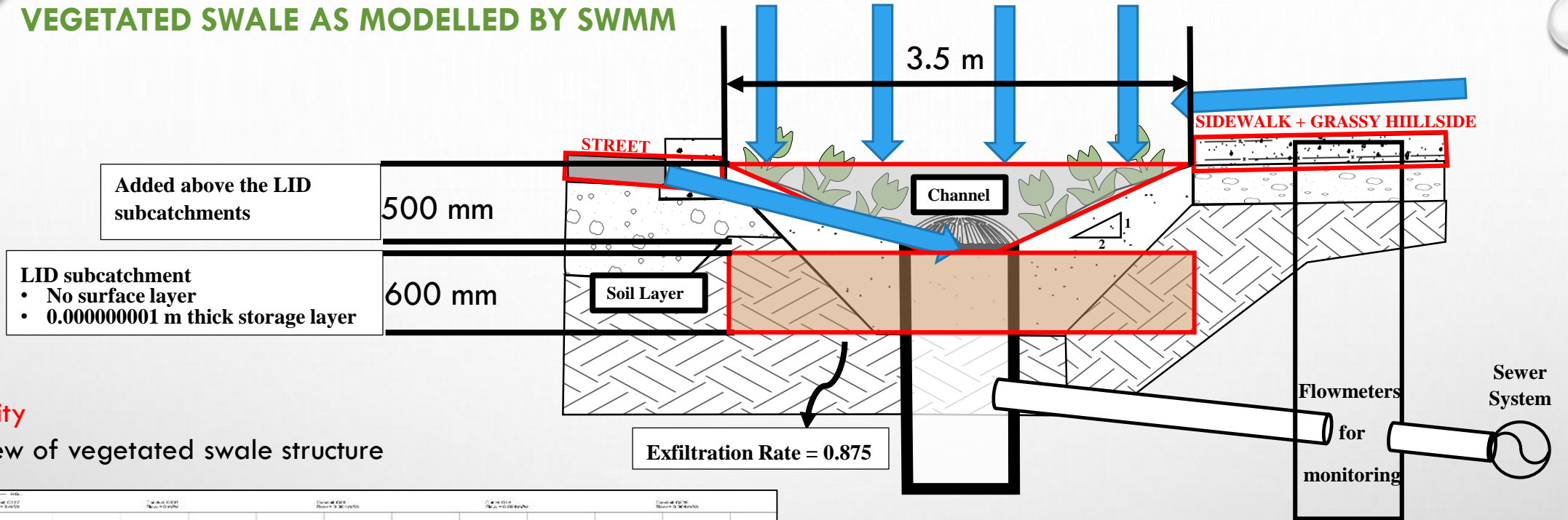
### CHANGES:

### CORRECT ASPECTS USING THE REAL AREA:

- Volume of **SOIL LAYER**
  - Real =  $127.94 \text{ m}^3$
  - SWMM =  $122.21 \text{ m}^3$

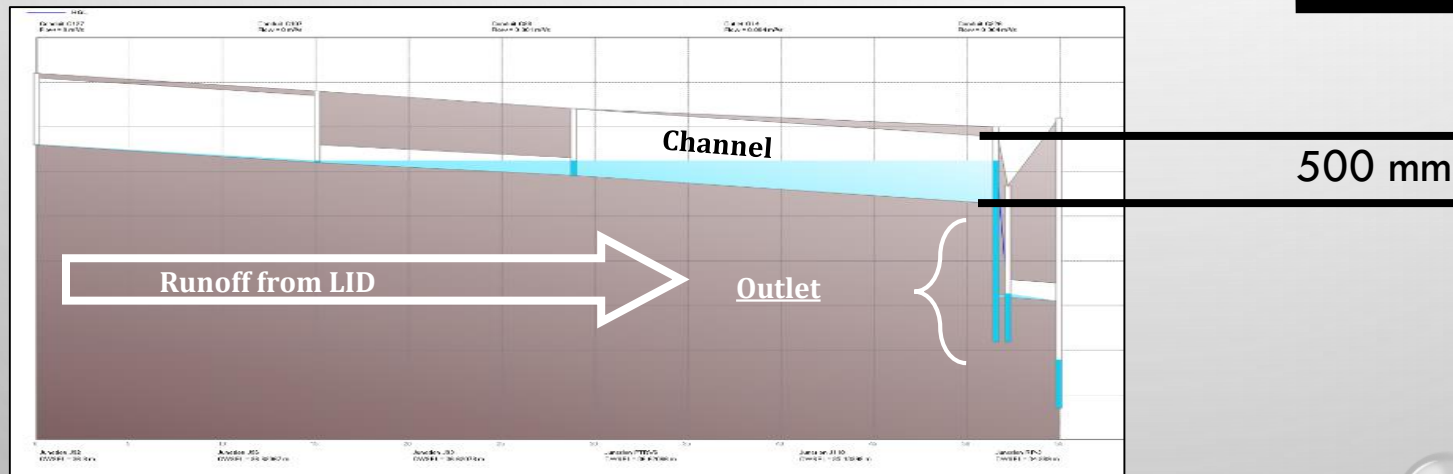
- Height of surface layer is adjusted to 250 mm so potential storage volume is accurate

## VEGETATED SWALE AS MODELLED BY SWMM



### Particularity

Profile view of vegetated swale structure



# INPUT FIELD DATA

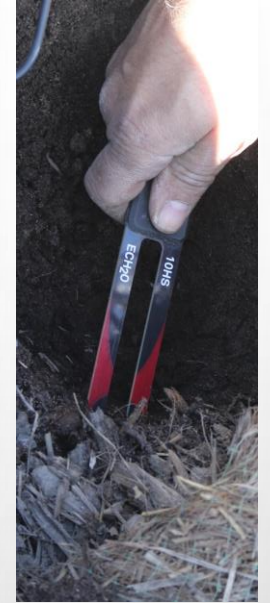
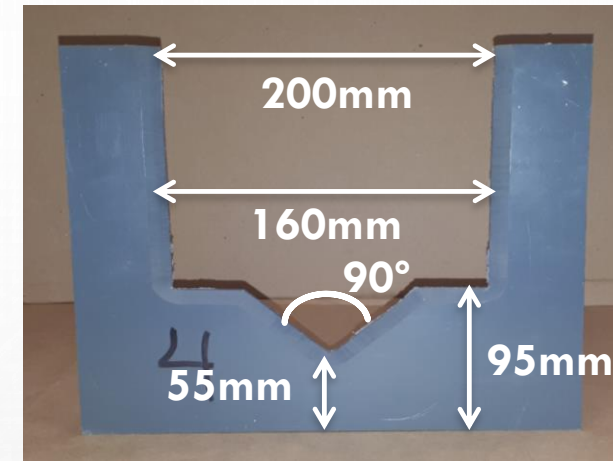
## WEATHER STATION:

- 79.2 cm from 47 precipitation events (April 18<sup>th</sup> – nov 5<sup>th</sup> 2019)
- Max and min daily Temperature data for climate file (evaporation calculations)

## FLOWMETERS AND WEIRS:

- Compound weirs (90° v-notch and rectangular)
- Standard calibration completed in the laboratory and verified in-situ
- Second measurement system = probe with a pressure transducer

## MOISTURE CONTENT PROBES



## GENERAL PARAMETERS

Parameter	Value	Source
Manning coefficient – impervious	0.01	(James et al., 2011)
Manning coefficient – pervious	0.1	(James et al., 2011)
D store imperv (mm)	1	(James et al., 2011)
D store perv (mm)	5	(James et al., 2011)
Zero Imperv (%)	25%	Default
Infiltration Model	Green-Ampt	--
Suction Head (mm)	166.8	Silt Loam (based upon geotechnical analysis of bore holes) (MDDEFP, 2014)
Conductivity (mm/hr)	6.6	
Moisture Deficit	0.501	

## LID PARAMETERS

Parameter	Value	Source
<b>Surface Layer</b>		
Berm Height (mm)	Swale 0	Project construction plans
	Bio 250	
Vegetation Volume (fraction)	0.1	(James et al., 2011)
Surface Roughness	0.3	(James et al., 2011)
<b>Soil Layer</b>		
Soil Thickness (mm)	600	Project construction plans
Soil Classification	<b>Silty Sand</b>	(García-Gaines & Frankenstein, 2015)
Hydraulic Conductivity $K_s$ (mm/hr)	91	(Rossman & Huber, January 2016)
Suction Head (mm)	50	(Rossman & Huber, January 2016)
Porosity (fraction)	Swale 0.467	Laboratory tests
	Bio 0.54	
Field Capacity	0.121	(Rossman & Huber, January 2016)
Wilting Point	0.057	(Rossman & Huber, January 2016)
Conductivity Slope (HCO)	44	(Rossman & Huber, July 2016)
<b>Storage Layer</b>		
Thickness (mm)	Swale 0	Project construction plans
	Bio 400	
Seepage Rate (mm/hr)	0.875	Field Tests
<b>Underdrain (Bio only)</b>		
Underdrain coefficient	152	Calculated
Drain exponent	0.5	(Rossman & Huber, July 2016)
Offset Height (mm)	200	Project construction plans

# SENSITIVITY ANALYSIS

The sensitivity of parameters was quantified using the relative sensitivity (James, 2005):

$$\text{Relative Sensitivity} = \frac{\partial \text{COF} / \text{COF}}{\partial p / p}$$

Where COF = computed objective function;

$p$  = parameter value.

The total outflow volume and peak flow were used as objective functions.

## Results:

Parameters influencing detention (peak flow):

- Hydraulic conductivity

Parameters influencing retention (total volume):

- Conductivity slope, evaporation and porosity

## Values of Relative Sensitivity

% change	+25%				+50%			
	Swale		Bioretention		Swale		Bioretention	
Basin	Total Volume	Peak Flow	Total Volume	Peak Flow	Total Volume	Peak Flow	Total Volume	Peak Flow
Manning Coefficient	-0.8%	-0.9%	-0.6%	-1.4%	0	0	0	0
Surface Slope	-1.0%	-1.9%	-0.4%	-0.5%	0	0	0	0
Porosity	-18.4%	0	-30.8%	0	-18.4%	0	-29.0%	0
Wilting Point	1.8%	0	0	0	1.9%	0	0	0
Conductivity	-3.8%	0	2.1%	102.6%	-3.4%	0	1.7%	86.5%
Conductivity Slope	24.7%	2.8%	9.9%	0	22.1%	1.9%	9.1%	0
Seepage Rate	-9.4%	-0.9%	-8.6%	0	-7.3%	-0.5%	-8.2%	-0.6%
Evaporation Rates	-20.7%	-0.9%	-30.5%	0	-20.7%	-1.4%	28.4%	0

# CALIBRATION TO SENSITIVE PARAMETERS

$$\text{Soil percolation speed} = \frac{K_{rs}}{e^{HCO}(\phi_2 - \theta_2)}$$

## VEGETATED SWALE:

- Outflow volume overestimation (retention metric);
  - Increase percolation speed to increase infiltration of runoff;
    - (+) hydraulic conductivity ( $K_s$ ) and (-) conductivity slope (HCO);
  - (+) porosity and (+) evaporation;

## BIORETENTION BASIN:

- ❑ Time to start of runoff dis-alignment and peak flow overestimation (detention metrics);
  - ❑ Increase percolation speed to align observed and simulated hydrographs;
    - ❑ (+)  $K_s$  and (-) conductivity slope
- Outflow volume overestimation (retention metric);
  - (+) porosity and (+) evaporation

Evaporation rates				
Source	April	May	June	July
Environment Canada averages from 1981 to 2010	0	4.2	4.6	4.6
Simulated in SWMM from climate file	0.5	2.9	3.7	4.7

## Evaluation of model efficiency

- NSE = The Nash-Sutcliffe coefficient used to assess specifically the predictive power of hydrological models (Nash & Sutcliffe, 1970). Performance required is  $NSE > 0.5$
- Error in effluent volume and peak flow < 25 %

## Optimal values (SWMM reference manual Vol 3 pg 127)

- $K_s$  = increased from 91 to 140 mm/hr
- Conductivity Slope (HCO) = reduced from 44 to 30

## Parametric Calibration Results

### VEGETATED SWALE:

**NSE = 0.206**

**33.9% ERROR VOL**

**25.3% ERROR PEAK**

### BIORETENTION BASSIN:

**NSE = -0.686**

**96.6% ERROR VOL**

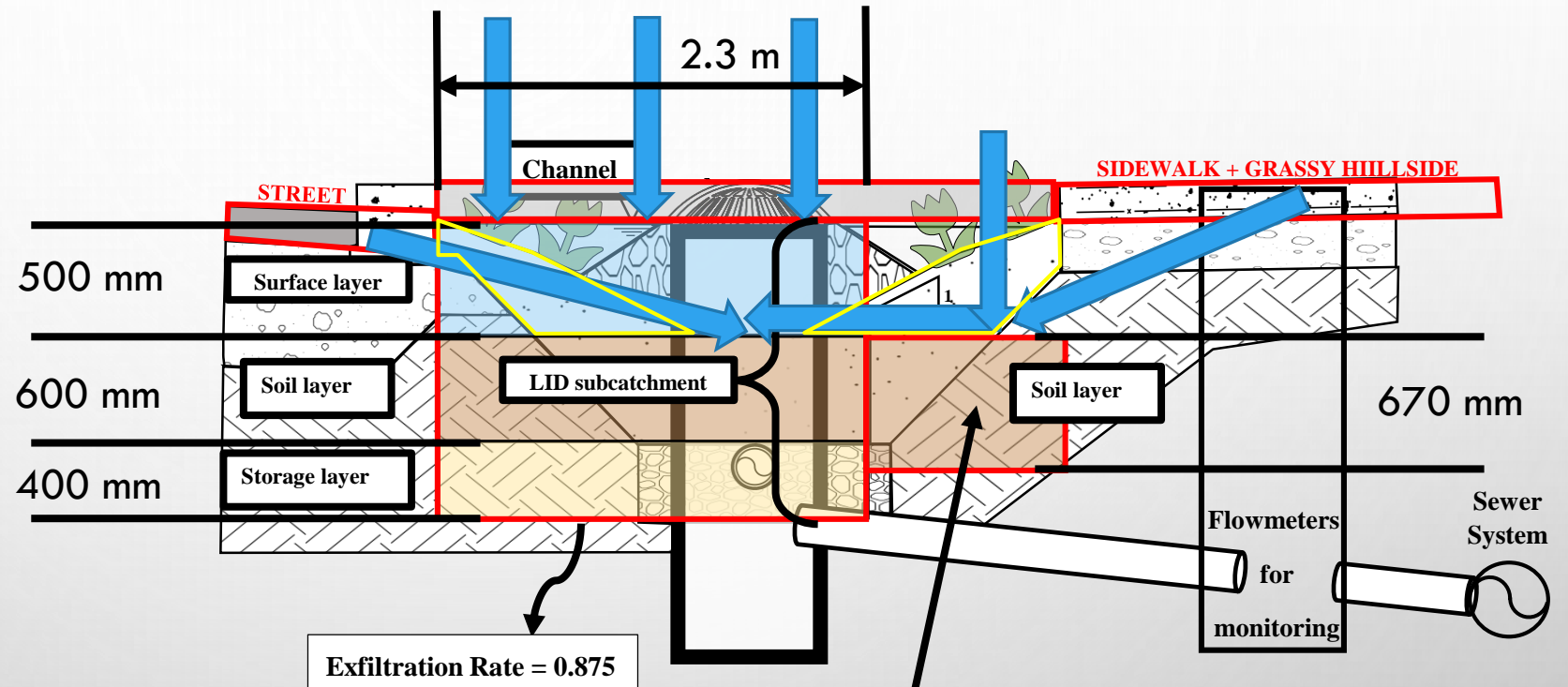
**25.4% ERROR PEAK**

## REDESIGN OPTIONS: CASE 1

## BIORETENTION BASIN

## CHANGES:

- KEEP REAL SURFACE LAYER HEIGHT 500 MM;
- ADJUST WIDTH TO MAKE SURFACE LAYER VOLUME ACCURATE BUT MORE TO SIMULATE FORM OF SOIL LAYER MORE ACCURATELY;
- ADDED A SEPARATE LID TO REPRESENT THE TOP SIDE SOIL (HIGHLIGHTED IN YELLOW);



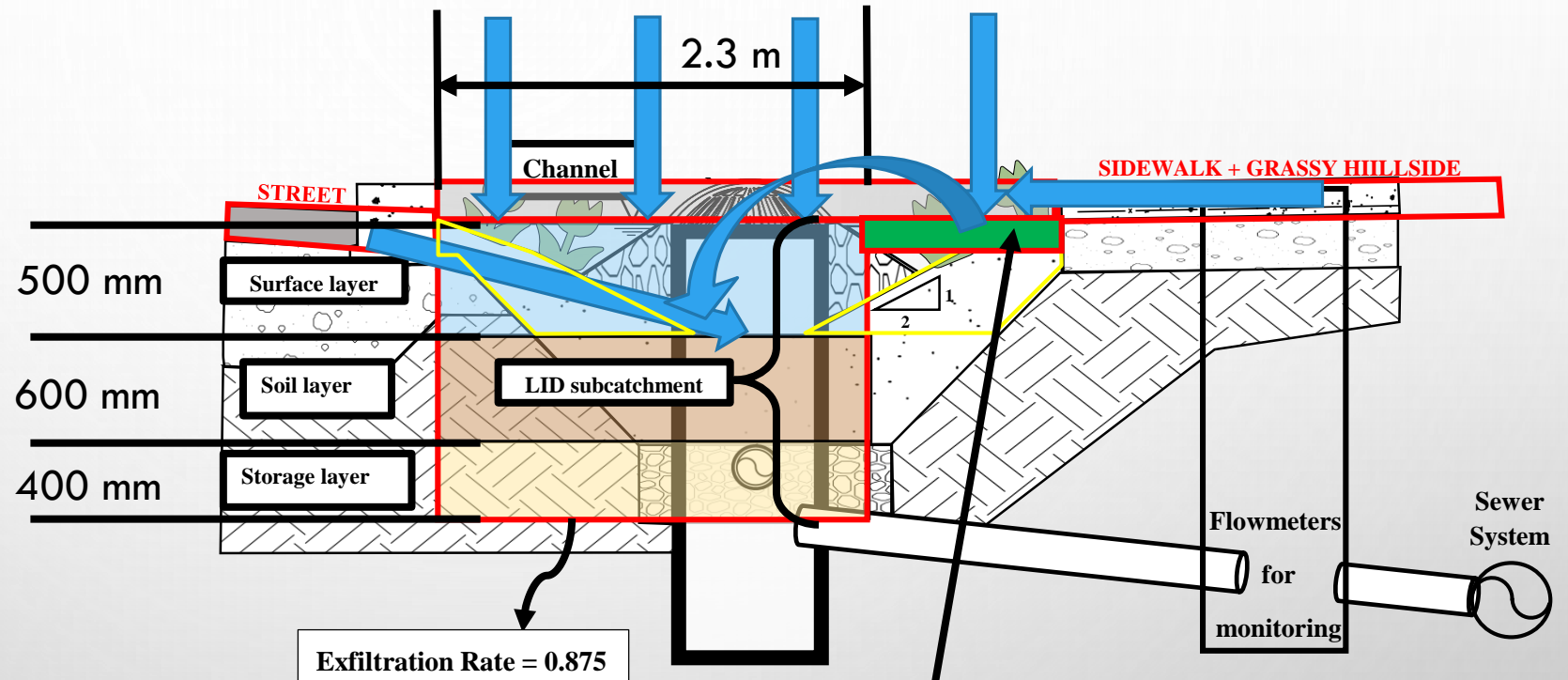
Additional LID to represent the top part of the soil layer in yellow

## REDESIGN OPTIONS: CASE 2

### BIORETENTION BASIN

#### CHANGES:

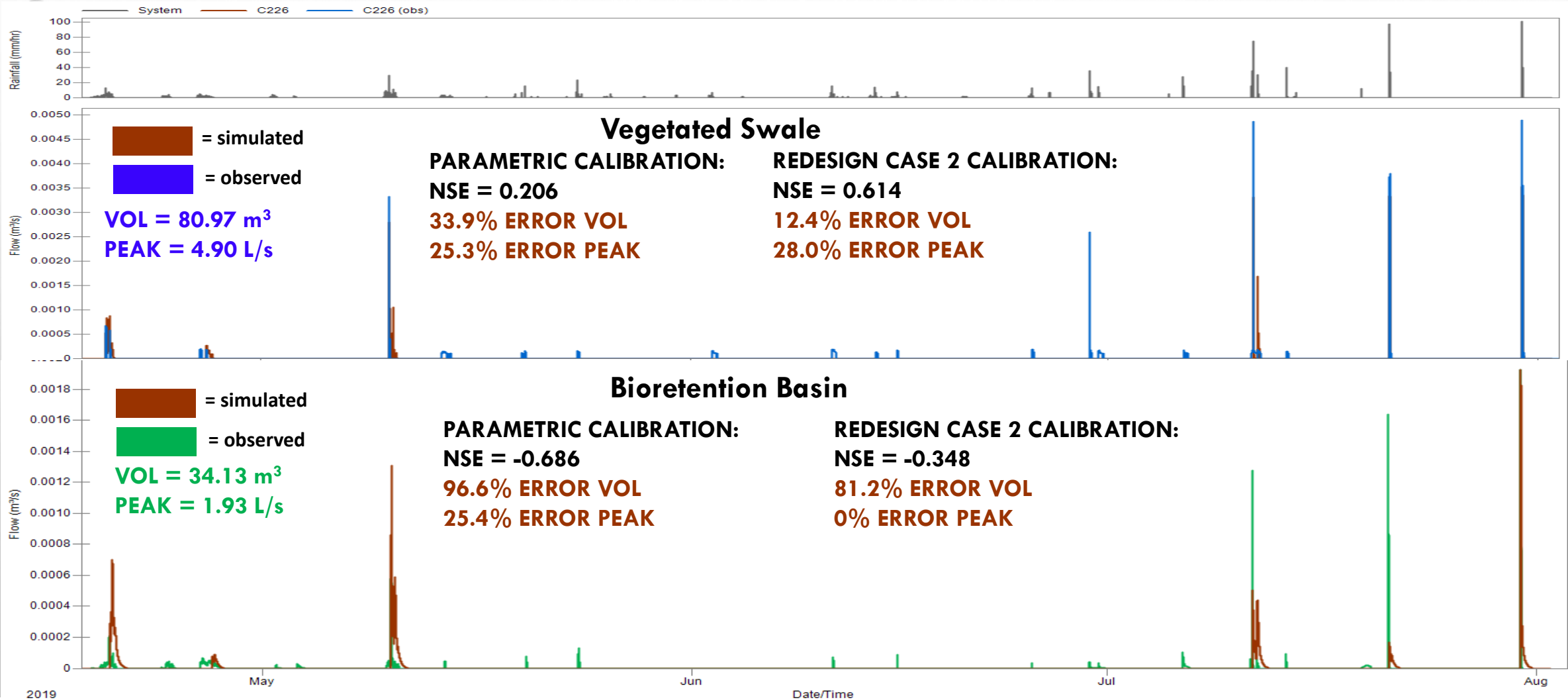
- KEEP REAL SURFACE LAYER HEIGHT 500 MM;
- ADJUST WIDTH TO MAKE SURFACE LAYER VOLUME ACCURATE BUT MORE TO SIMULATE FORM OF SOIL LAYER MORE ACCURATELY;
- ADDED A SEPARATE **SUBCATCHMENT** TO REPRESENT THE TOP SIDE SOIL (HIGHLIGHTED IN YELLOW);



Additional subcatchment to represent the top soil (completely pervious with green-ampt parameters of suction head 50; conductivity 140 and initial deficit of 0.463)

# CALIBRATED RESULTS – REDESIGN CASE 2

CONTINUOUSLY FROM APRIL 18<sup>TH</sup> – JULY 30<sup>TH</sup>



2019

May

Jun



Date/Time

Jul

Aug

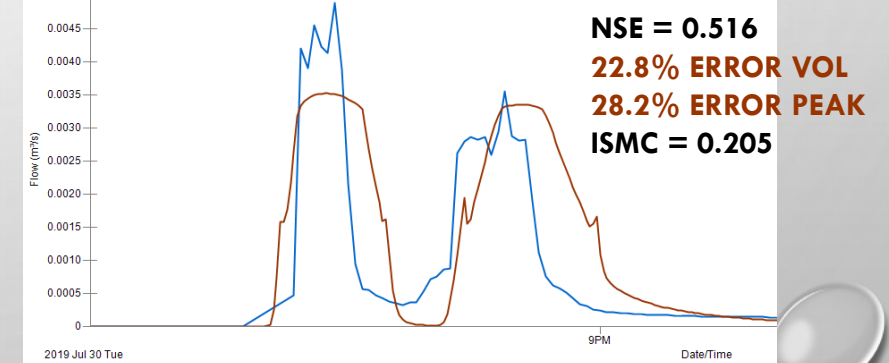
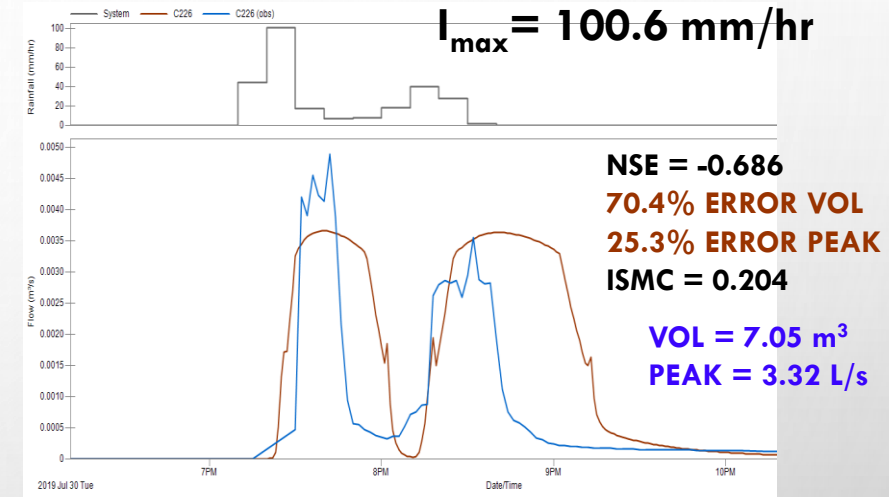
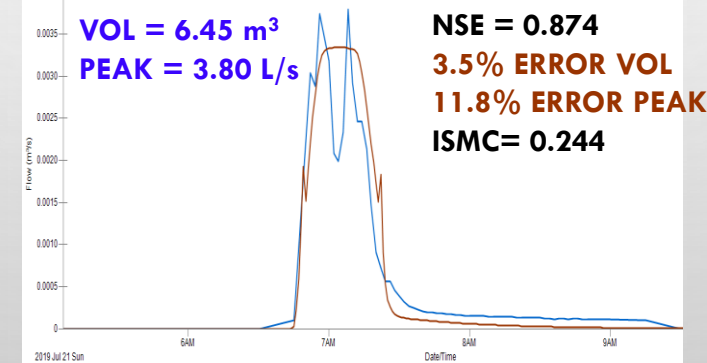
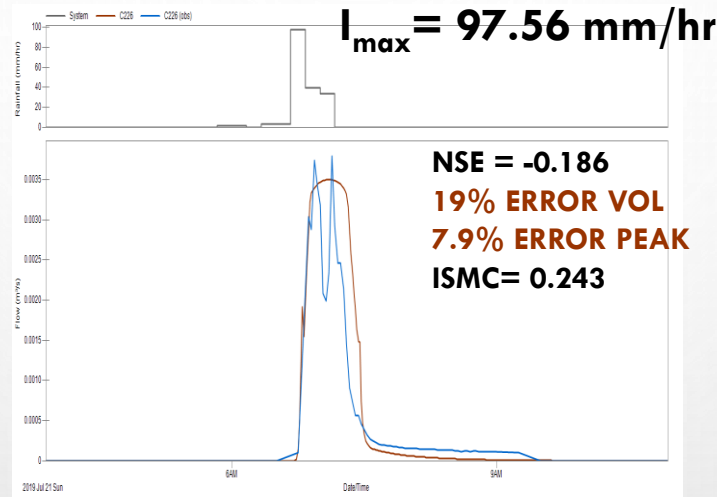
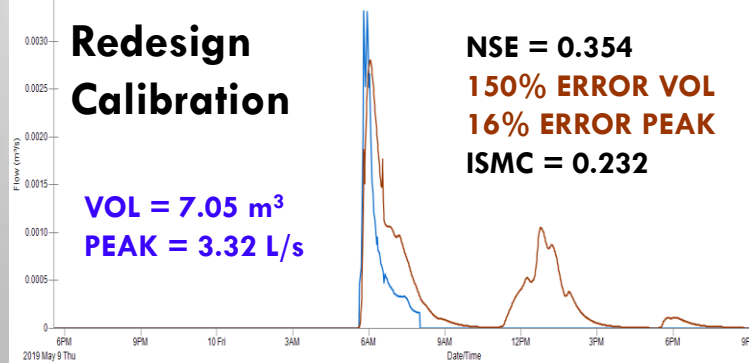
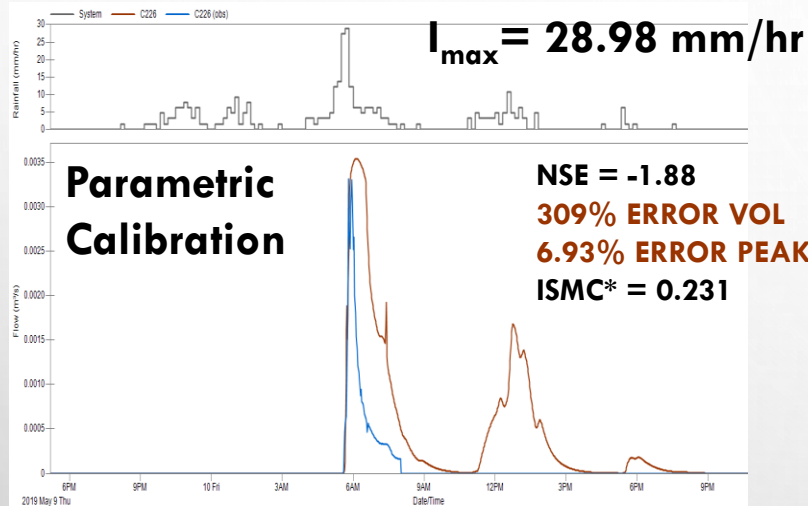
# CALIBRATED RESULTS – REDESIGN CASE 2 – VEGETATED SWALE

MAY 9<sup>TH</sup> : 57.12 mm in 24 hrs  
with 6.29 antecedent dry days

 = simulated  
 = observed

JULY 21<sup>ST</sup> : 29.97 mm in 1h20min  
with 2.70 antecedent dry days



JULY 30<sup>TH</sup> : 43.68 mm in 1h30min  
with 9.50 antecedent dry days



\*ISMC = Initial Soil Moisture Content

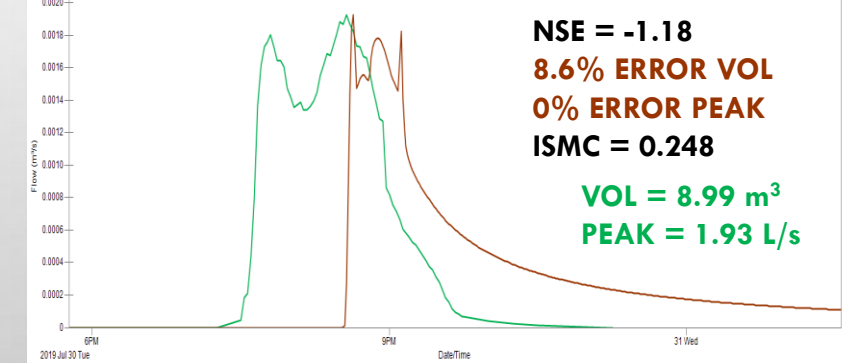
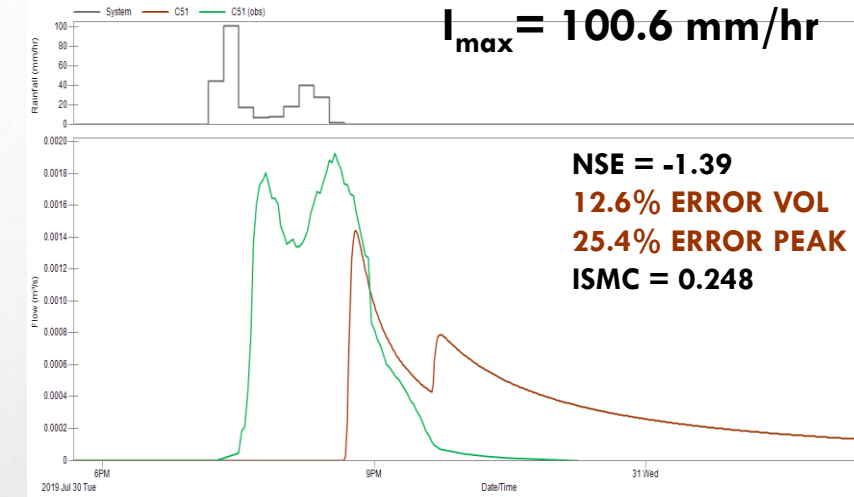
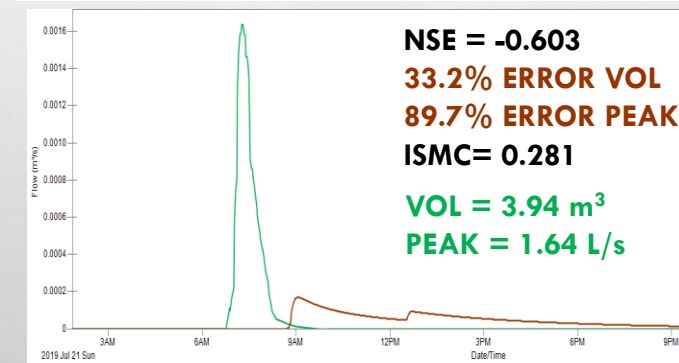
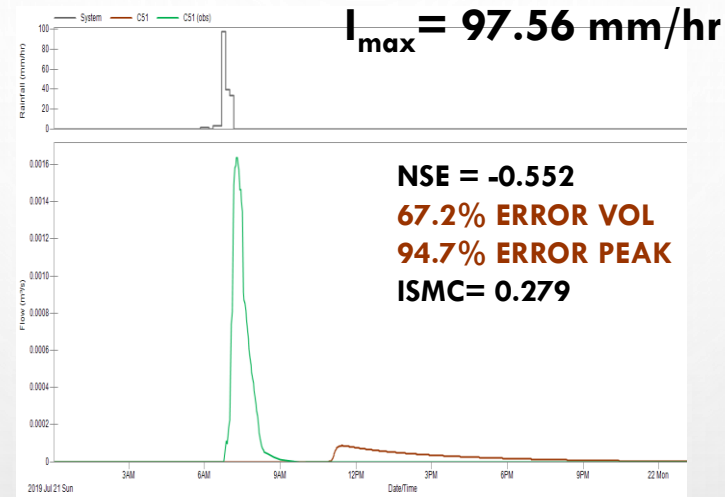
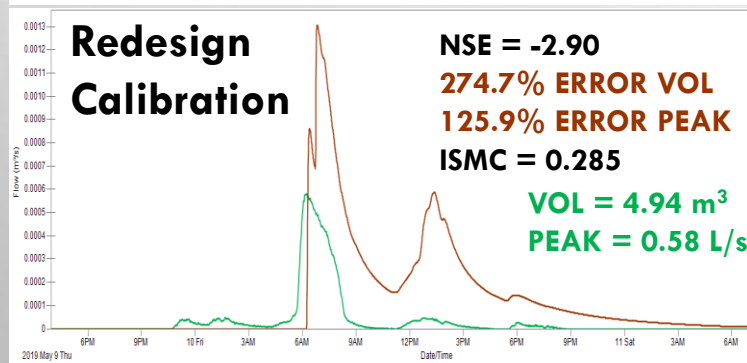
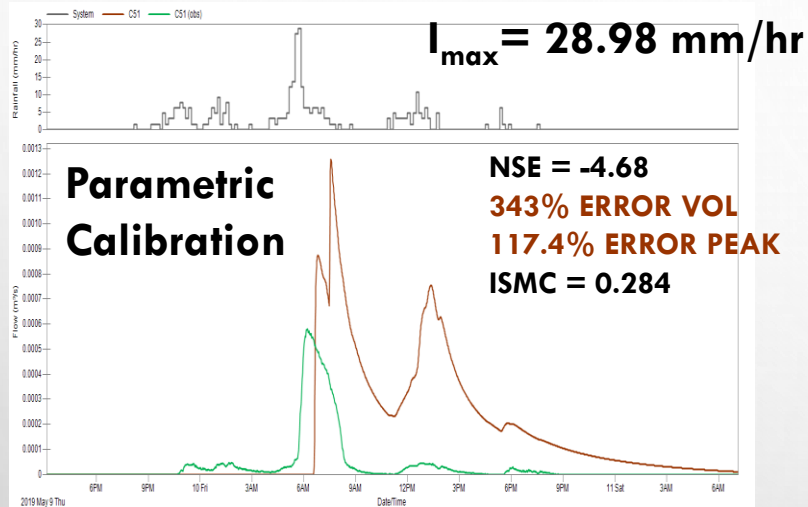
# CALIBRATED RESULTS – REDESIGN CASE 2 – BIORETENTION BASIN

MAY 9<sup>TH</sup> : 57.12 mm in 24 hrs  
with 6.29 antecedent dry days

 = simulated  
 = observed

JULY 21<sup>ST</sup> : 29.97 mm in 1h20min  
with 2.70 antecedent dry days

JULY 30<sup>TH</sup> : 43.68 mm in 1h30min  
with 9.50 antecedent dry days

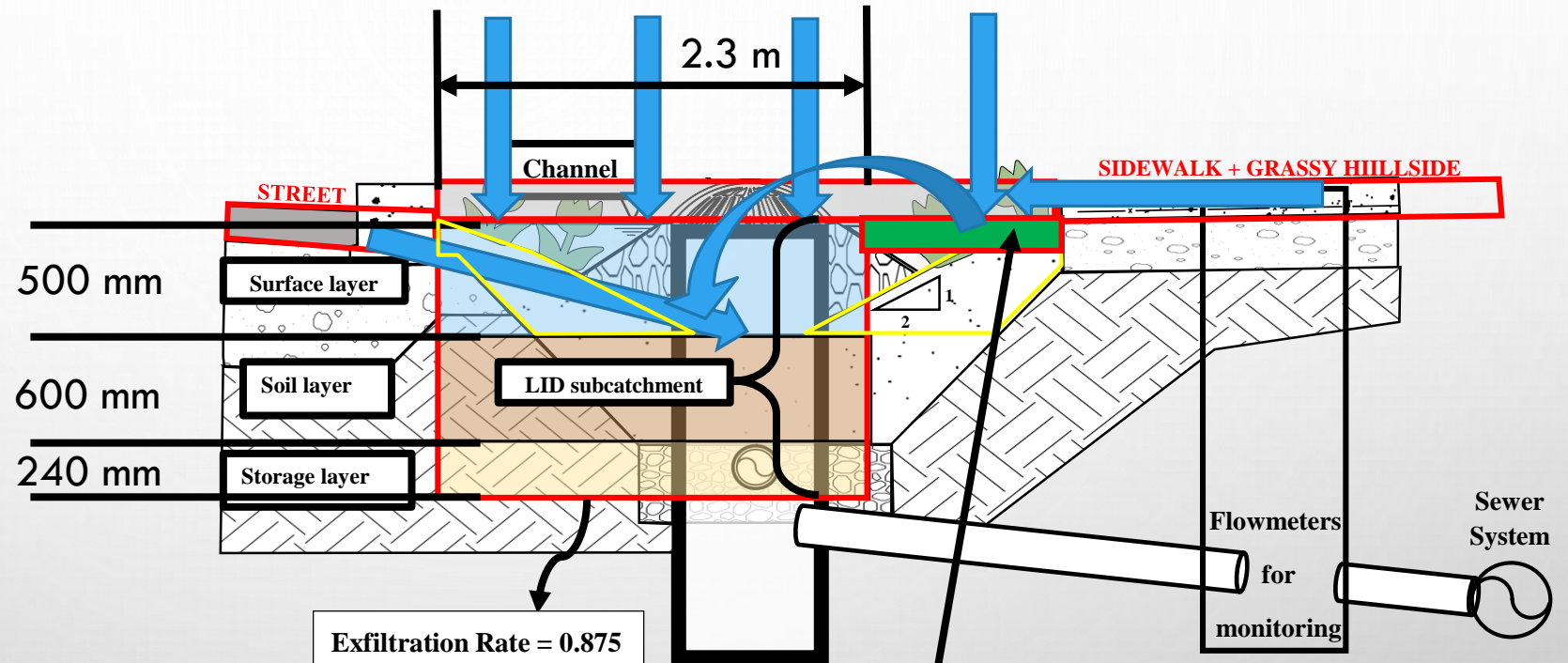


## REDESIGN OPTIONS: CASE 3

### CHANGES:

- KEEP REAL SURFACE LAYER HEIGHT 500 MM;
- ADJUST WIDTH TO MAKE SURFACE LAYER VOLUME ACCURATE BUT MORE TO SIMULATE FORM OF SOIL LAYER MORE ACCURATELY;
- ADDED A SEPARATE **SUBCATCHMENT** TO REPRESENT THE TOP SIDE SOIL (HIGHLIGHTED IN YELLOW);
- **MAKE STORAGE VOLUME CORRECT BY REDUCING HEIGHT TO 240 MM;**

### BIORETENTION BASIN



Additional subcatchment to represent the top soil (completely pervious with green-ampt parameters of suction head 50; conductivity 140 and initial deficit of 0.463)



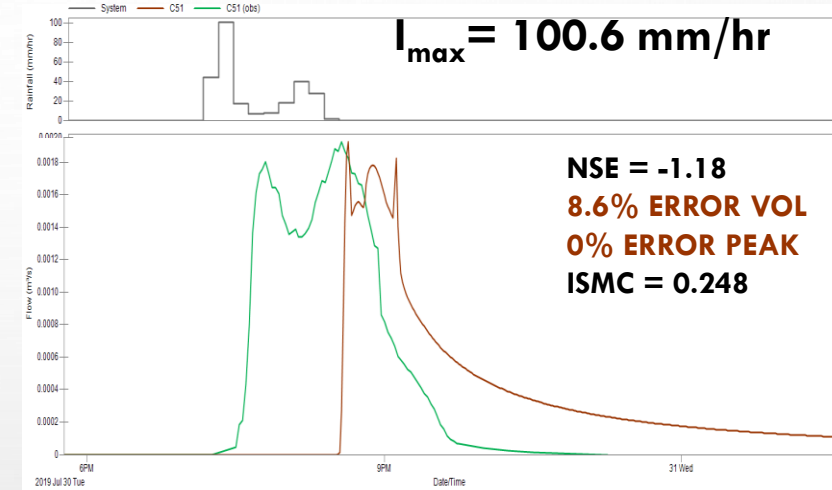
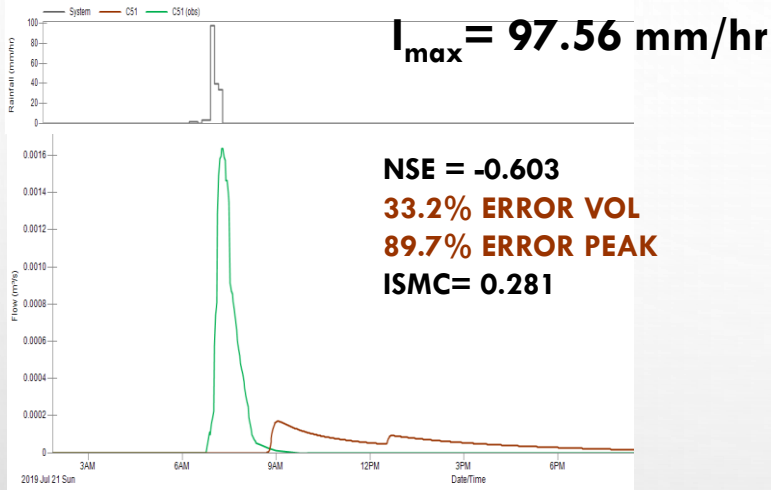
# CALIBRATED RESULTS – REDESIGN CASE 3 – BIORETENTION BASIN

**JULY 21<sup>ST</sup> : 29.97 mm in 1h20min**  
with 2.70 antecedent dry days

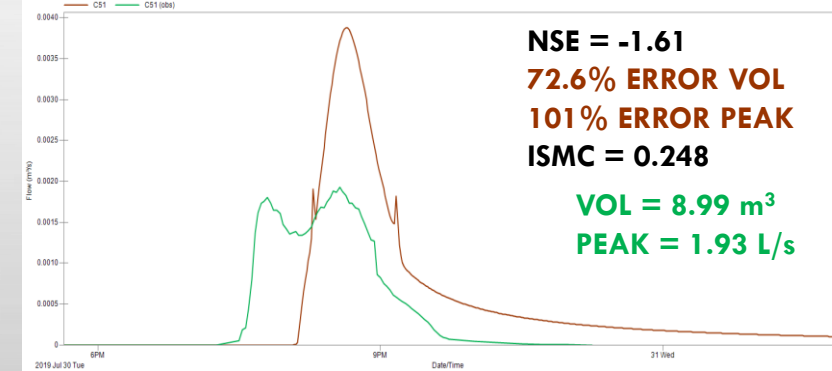
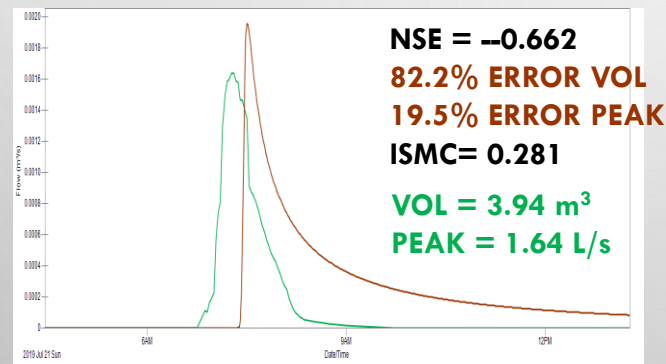
= simulated  
 = observed

**JULY 30<sup>TH</sup> : 43.68 mm in 1h30min**  
with 9.50 antecedent dry days

**Redesign  
Calibration  
Case 2**



**Redesign  
Calibration  
Case 3**



# CONCLUSIONS

- Vegetated swale vs bioretention performance
- Model vs observed data performance
- Contradiction in timing of outflow hydrographs and volume ejected
- Complex nature of the soil

## **Assuming observed data is correct**

- The complexity of soil behaviour is not completely captured by SWMM LID bioretention control
- The SWMM bioretention cell is accurate and it is the inflow that is being overestimated
- Liberation of soil retention capacity due to evaporation is not fully capture by SWMM

## **Assuming the model results are correct**

- Error in flow values derived from the weir calibration curves and the height of runoff measured by the probes

Note: It is unlikely that the timing of the observed exit hydrographs is incorrect

# REFERENCES

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[https://climat.meteo.gc.ca/climate\\_normals/results\\_1981\\_2010\\_f.html?searchType=stnName&txtStationName=Montr%C3%A9al&searchMethod=contains&txtCentralLatMin=0&txtCentralLatSec=0&txtCentralLongMin=0&txtCentralLongSec=0&stnID=5415&dispBack=0](https://climat.meteo.gc.ca/climate_normals/results_1981_2010_f.html?searchType=stnName&txtStationName=Montr%C3%A9al&searchMethod=contains&txtCentralLatMin=0&txtCentralLatSec=0&txtCentralLongMin=0&txtCentralLongSec=0&stnID=5415&dispBack=0)
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THANK YOU FOR LISTENING!

**QUESTIONS ? SUGGESTIONS?**

# CONCLUSIONS

Based on the model results, the bio-retention basin performance is superior to the vegetated swale however both basins performance's are inferior to the results from the observed data. Based on the observed data, the bio-retention basin reacts quickly to the rainfall event however is still able to retain a large amount of volume which seems contradictory. In the case of the model, it is not able to simulate both behaviors. This means that if the outflow is to be reduced, the alignment of the hydrographs will be lost and if the latter is prioritized, this leads to an overestimation of the volume. It is possible the model is too simple a representation of the complex nature of the soil and it not able to capture both penomenon simulatenously.